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### A GENERALIZED CORRELATION FOR THE EFFECT

### OF PRESSURE ON THE DIFFERENCE IN HEAT CAPACITIES

OF GASES

BY

### LEON BLEICH

### A THESIS SUBMITTED TO THE FACULTY OF THE DEPARTMENT OF CHEMICAL ENGINEERING OF NEWARK COLLEGE OF ENGINEERING

### IN PARTIAL FULFILLMENT OF THE REQUIREMENTS FOR THE DEGREE

OF

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### NEWARK, NEW JERSEY

### 1958

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#### SUMMARY

A generalized correlation is presented for the difference in heat capacities at constant pressure and constant volume,  $C_p$ - $C_v$ , as a function of reduced pressure with parameters of reduced temperature. The correlation covers a pressure range of  $p_r = 0.2$  to  $p_r = 15.0$  and a temperature range of  $T_r = 1.0$  to  $T_r = 5.5$ . The correlation was based on values of  $C_p$ - $C_v$  calculated from the Benedict - Webb - Rubin Equation of State for five hydrocarbons, namely, methane, ethylene, ethane, propane, and n-butane.

The results show that  $C_p-C_V$  approaches the universal gas constant, R, for all temperatures as the pressure approaches zero. In general, at any particular pressure, the value for  $C_p-C_V$  decreases with increasing temperature. The average deviation of the generalized correlation from the data on which it was based is  $\pm 0.93\%$ . Deviations as high as 8% were found in the region of very high reduced pressure. A comparison has been made with an earlier correlation presented by Edmister. The relative accuracies of the two correlations have been discussed. A comparison has also been made with data for nitrogen and carbon monoxide. The results indicate that this correlation can be used not only for hydrocarbons, but for other non-polar or slightly polar gases as well.

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### INTRODUCTION

Thermodynamic data, at elevated temperatures and pressures, are becoming more essential for design purposes in both the chemical and petroleum fields.

Work sponsored by the American Petroleum Institute as Research Project 44 has reported heat capacities in the ideal gaseous state for many of the hydrocarbons  $(\underline{1})$ . Very little actual experimental heat capacity data are available at high pressures. Although methods have been developed to accurately calculate heat capacities; these methods are often quite tedious and time consuming. To alleviate this problem the design engineer uses generalized correlations when actual data are not available. These correlations are developed in such a manner so as to be applicable to any gas.

It is the purpose of this work to submit a generalized correlation for  $C_p-C_v$ , in graphical form, to complement earlier work on heat capacities carried out at the Newark College of Engineering.

### Early Generalized Correlation for Cp-Cy:

The first presentation of this type was prepared in graphical form by Wayne C. Edmister (2). The basis for his correlation is the difference between the ideal and actual gas volume,  $\infty$ . This difference is defined as the Lewis and Randall volume residual quantity and is expressed by the equation  $\infty = RT/P - V$  (3). The residual quantity,  $\infty$ , adapts itself well to graphical methods and has been discussed by Deming and Shupe (4)(5). By setting  $\infty = \infty_r \infty_c$ ,  $P = P_r P_c$ , and  $T = T_r T_c$ , the following modified reduced equation of state is obtained:

$$\frac{\mathbf{v}}{\boldsymbol{\alpha}_{\mathbf{o}}} = \frac{\mathbf{R}\mathbf{T}_{\mathbf{r}}\mathbf{T}_{\mathbf{o}}}{\mathbf{P}_{\mathbf{r}}\mathbf{P}_{\mathbf{o}}\boldsymbol{\alpha}_{\mathbf{o}}} - \boldsymbol{\alpha}_{\mathbf{r}}$$

The equation for the difference in heat capacities is:

$$c_{p}-c_{v} = -T \frac{(\partial V/\partial T)_{p}^{2}}{(\partial V/\partial P)_{m}} \qquad (\underline{6}) \quad (p.461)$$

When reduced units and  $\sigma_r$  are introduced this equation becomes:

$$c_{p}-c_{v} = -T_{r} \frac{\left[R/P_{r} - K_{2} \left(\partial \alpha_{r} / \partial T_{r}\right)_{P_{r}}\right]^{2}}{\left[RT_{r} / P_{r}^{2} - K_{2} \left(\partial \alpha_{r} / \partial P_{r}\right)_{T_{r}}\right]}$$

where  $K_2 = \alpha_c P_c/T_c$ . The value of  $K_2$  was found to be substantially constant varying from 1.41 to 1.47 and averaging 1.44 for all components except carbon dioxide and hydrogen (Z). The derivatives  $(\partial \alpha_r/\partial T_r)_{P_r}$  and  $(\partial \alpha_r/\partial P_r)_{T_r}$  were determined graphically from large scale plots of  $\alpha_r$  against  $T_r$  isobars and  $\alpha_r$  against  $P_r$  isotherms. Edmister has tabulated values for these derivatives and has presented a generalized correlation in graphical form for  $C_p-C_v$  as a function of reduced pressure, with parameters of reduced temperature (2)(8). Sixteen parameters of reduced temperature were presented varying from  $T_r = 0.8$  to  $T_r = 2.5$ . Reduced pressure ranged between the limits of  $P_r = 0.04$  to  $P_r = 4.0$ .

## $C_p-C_v$ Data Based on the Benedict - Webb - Rubin Equation of State:

Since it is extremely difficult to make direct experimental heat capacity measurements accurately, an alternative approach must be used. An indirect, but fairly accurate, method is to use an equation of state which will reproduce with reasonable accuracy p-V-T relationships.

The Benedict - Webb - Rubin Equation is considered to be the best equation of state developed to date. It was developed primarily for hydrocarbons to reproduce most accurately p-V-T relations of gases.

Although the equation is extremely complex, employing eight constants, it provides a direct method of calculating the desired thermodynamic function. The equation is continuous for both the liquid and gaseous states and describes most accurately p-V-T data up to about 1.8

times the critical density.

The Newark College of Engineering has undertaken a program to calculate  $C_p-C_p^*$  over a large range of temperature and pressure for various gases using the Benedict -Webb - Rubin Equation of State. The first five gases studied are reported in the following theses:

- 1. "Isobaric Heat Capacity of Methane over a Wide Range of Temperature and Pressure" (9)
- 2. "Isobaric Heat Capacity of Ethylene over a Wide Range of Temperature and Pressure" (10)
- 3. "Heat Capacities of Ethane over a Wide Range of Temperature and Pressure" (11)
- 4. "Isobaric Heat Capacity of Propane over a Wide Range of Temperature and Pressure" (12)
- 5. "Isobaric Heat Capacity of n-Butane over a Wide Range of Temperature and Pressure" (13)

In using the Benedict - Webb - Rubin Equation to calculate  $C_p-C_p^*$ , values of  $C_p-C_v$  and  $C_v-C_v^*$  are obtained as intermediate quantities.

Weiss has used the data reported in these five theses to prepare a graphical generalized correlation for  $C_p=C_p^*$  (14).

De Laney has also used these data to calculate the ratio of  $C_p/C_v$  for the five gases previously investigated (15). Since the heat capacity ratio,  $C_p/C_v$ , cannot be generalized, the work submitted by De Laney is applicable only to the

### specific gases investigated.

In this work, the data available in the original five theses has been used to prepare a generalized correlation for  $C_p-C_v$ . The work presented here, when used in conjunction with the generalized correlation presented by Weiss, will permit an investigator to estimate values for  $C_p$ ,  $C_v$ , and the ratio of  $C_p/C_v$ . To find one or more of these terms it is necessary to know only the critical temperature and pressure and  $C_p^*$  for the given component. Values for these terms have been compiled for most hydrocarbons by the American Petroleum Institute as Research Project 44 (1).

### DERIVATION OF THE EQUATION FOR Cp-Cv FROM THE BENEDICT - WEBB - RUBIN EQUATION OF STATE

The Benedict - Webb - Rubin Equation is presented by the authors in the following form (9):

(1) 
$$P = RTd + (B_0RT - A_0 - C_0T^{-2})d^2 + (bRT - a)d^3$$
  
+  $a \propto d^6 + cd^3(1 + \chi d^2)T^{-2}e^{-\chi d^2}$ 

Equation (i) may be expressed in terms of volume rather than density as follows:

(11) 
$$P = RTV^{-1} + (B_0RT - A_0 - C_0T^{-2})V^{-2} + (bRT - a)V^{-3} + a \propto V^{-6} + oV^{-3}(1 + VV^{-2})T^{-2}e^{-(VV^{-2})}$$

(111)  $C_{p}^{*}-C_{v}^{*}=R$ ; for an ideal gas.

From Hougen and Watson (6) (p.461) for an actual gas:

(iv) 
$$C_p - C_v = -T(\partial P / \partial T)_v^2 / (\partial P / \partial V)_T$$

Performing the indicated operation of Equation (iv) on Equation (ii):

(v) 
$$(\partial P/\partial T)_{V} = RV^{-1} + (B_{0}R + 2C_{0}T^{-3})V^{-2} + bRV^{-3}$$
  
-  $2cV^{-3}T^{-3}(1 + V^{-2})e^{-VV^{-2}}$ 

(v1) 
$$(\partial P/\partial V)_{T} = -RTV^{-2} - 2V^{-3}(B_0RT - A_0 - C_0T^{-2})$$
  
-  $3V^{-4}(bRT - a) - 6a \ll V^{-7}$   
+  $cT^{-2}e^{-x}V^{-2}(-3V^{-4} - 3xV^{-6} + 2x^2V^{-8})$ 

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Substituting Equations (v) and (vi) in Equation (iv):

(v11)  

$$C_{p}-C_{v} = -T \frac{\left[Rv^{-1} + (B_{0}R + 2C_{0}T^{-3})v^{-2} + bRv^{-3}\right]^{2}}{\left[-2cv^{-3}T^{-3}(1 + vv^{-2})e^{-vv^{-2}}\right]^{2}} \frac{1}{\left[-RTv^{-2} - 2v^{-3}(B_{0}RT - A_{0} - C_{0}T^{-2})\right]^{2}} \frac{1}{\left[-RTv^{-2} - 2v^{-3}(B_{0}RT - A_{0} - C_{0}T^{-2})\right]^{2}} \frac{1}{\left[-RTv^{-2}e^{-vv^{-2}}(-3v^{-4} - 3vv^{-6} + 2v^{2}v^{-8})\right]^{2}}$$

### METHOD OF CALCULATION

Previous investigators, at the Newark College of Engineering, have already calculated values for  $C_p-C_v$ over a large range of temperature and pressure using the Benedict - Webb - Rubin Equation (9)(10)(11)(12)(13). The values obtained were specific for each gas studied. The constants used in the Benedict - Webb - Rubin Equation are also specific for each gas and are shown in Table 1.

A typical example which shows how the data were treated to obtain a generalized correlation is described below. T.A. Reiter presented values for  $C_p-C_v$  for ethane over a wide range of temperature and pressure (11). At 150°F., Reiter presented the following data:

$t(^{O_{\rm F}})$	<u>p(psia)</u>	cp-cv(Btu/#-OF)
150	744.0	0.3028
-	556.5	0.1888
	374.0	0.1262
	238.7	0.09814
	125.0	0.08079

The generalized correlation presented as a result of this work is prepared in graphical form as a plot of  $C_p-C_v$  (expressed in molal units) vs. reduced pressure for a number of parameters of reduced temperature. Therefore it is necessary to convert the data shown above to these consistent units. The values used for the critical temperature, critical pressure, and molecular weight are shown in Table 2 and were obtained from the American Petroleum Institute Research Project 44 (1). The following values were used for ethane:

$$T_c = 549.77$$
 °R.  
 $p_c = 708.3 psia$   
M.W. = 30.068 #/#-Mol.

Using the constants shown above for ethane, the desired units of reduced temperature and pressure and molal heat capacity difference were calculated using the following equations:

$$T_{r} = \frac{T}{T_{c}} = \frac{t(OF) + 459.69}{549.77}$$
$$p_{r} = \frac{p}{p_{c}} = \frac{p(psia)}{708.3}$$

 $C_{p}=C_{v}(Btu/\#-Mol^{O}F) = c_{p}-c_{v}(Btu/\#-^{O}F) \times M.W.(\#/\#-Mol)$ =  $c_{p}-c_{v}(Btu/\#-^{O}F) \times 30.068$ 

The data for the difference in heat capacities of ethane for the 150°F. isotherm becomes:

<u> </u>	<u>p</u>	$\frac{C_p - C_v (Btu/#-Mol_{oP})}{C_p - C_v (Btu/#-Mol_{oP})}$
1.109	1.050 0.786 0.528 0.337 0.1765	9.10 5.68 3.79 2.951 2.429

Calculations similar to those shown above were made for the other isotherms of ethane and also for ethylene, propane, and n-butane. For the latter three gases values of  $C_p-C_v$  were expressed in units of Liter-Atm/Gm-Mol-<sup>O</sup>K. These units were converted to Btu/#-Mol-<sup>O</sup>F by multiplying by 24.2021. Values of  $C_p-C_v$  for methane were not directly available. These data were calculated from the values of  $C_p-C_p^*$  and  $C_p/C_v$  given by Weiss and De Laney, respectively, and the values of  $C_p^*$  (14)(15)(1). The calculated data for each gas is given in Tables 3-7. These data were plotted as a function of reduced pressure, with parameters of reduced temperature. An example of the type of curves obtained is illustrated for ethane in Figure 1.

In order to best utilize the data to prepare a generalized correlation, the data were converted into uniform parameters of reduced pressure and temperature. A total of fifteen isobars were chosen. These are numerically identical with the isobars chosen by Weiss since the two correlations may often be used together. The isobars selected are:

 $p_r = 0.2, 0.3, 0.4, 0.6, 0.8, 1.0, 1.5, 2, 3, 4, 6, 8, 10, 12, and 15.$ 

As an example, the following data are obtained for ethane from Figure 1, for the isobar  $p_n = 6.0$ :

Ethane:  $p_r = 6.0$ 

Tr	1.564	1.746	1.928	2.291	2.655	3.38
Cp-Cv	7.01	5.77	4.80	3.77	3.18	2.64

Values of  $C_p-C_v$  versus reduced temperature for parameters of reduced pressure were tabulated in a similar manner for all five gases and are presented in Tables 8-12.

The generalized correlation was prepared using Tables 8-12 as a basis. Values of Cp-Cy were plotted against reduced temperature, using the data for all five gases, for each parameter of reduced pressure. The type of plot obtained is illustrated in Figure 2 for a reduced pressure of 6.0. This figure also shows the excellent agreement between the data and the average line drawn. The family of curves obtained is shown in Figure 3. This plot is actually a generalized correlation of  $C_p - C_w$ versus reduced temperature with parameters of reduced pressure. This plot is not very convenient to use because of the crossing of lines. A more useful plot is one of  $C_{D}-C_{V}$  versus reduced pressure with parameters of reduced temperature, since crossing of lines is eliminated. In order to prepare this plot an arbitrary set of isotherms must be chosen. Eighteen isotherms were selected ranging from  $T_r = 1.0$  to  $T_r = 5.5$ . These are also numerically equal to the isotherms chosen by Weiss. Values of  $C_p-C_v$ are obtained where the isotherms intersect with each of

the previously selected isobars.

As an example, for  $p_r = 6.0$ , from either Figure 2 or Figure 3, the following data are obtained:

Tr	1.6	1.75	2.0	2.25	2.5	2.75
c <sub>p</sub> -c <sub>v</sub>	6.85	5.79	4.62	3.86	3.39	3.06
Tr	3.0	3.5	4.0	4.5	5.0	5.5
C <sub>D</sub> -C <sub>V</sub>	2.85	2.58	2.42	2.32	2.25	2.21

Similar tabulations were made for each parameter of reduced pressure. These data are presented in Table 13. This table contains the coordinates for the generalized correlation of  $C_p-C_v$  versus reduced pressure, with parameters of reduced temperature. The data from Table 13 are plotted in Figure 4. This figure contains the desired generalized correlation.

### Comparison of Generalized Correlation with Original Data:

To determine quantitatively the deviation of the generalized correlation from the data used in its preparation, the original data contained in Tables 3-7 were representatively sampled. For each gas at least two extremes and a mean reduced temperature were chosen, and then, for each reduced temperature, at least two extremes and a mean reduced pressure were tabulated along with their corresponding values of  $C_p-C_v$ . Corresponding

to each value of reduced temperature and pressure selected, values of  $C_p-C_w$  were read from the generalized correlation presented in Figure 4.

The following example, for ethane, illustrates the method of sampling and manner in which the generalized correlation was compared with the original data:

I	II	III	IV	V	VI
Tr	<u> </u>	<u>Calc.</u>	<u> </u>	Difference	% Deviation
1.291	0.2028	2.306	2.30	-0.006	-0.3
	1.006	4.28	4.35	0.07	1.6
	1.397	5.91	6.10	0.19	3.2
1.746	0.2866	2.169	2.17	0.001	0.05
	1.512	3.12	3.12	0.00	0.0
	2.938	4.36	4.32	-0.04	-0.9
	12.81	5.54	5.55	0.01	0.2
2.291	0.380	2.107	2.10	-0.007	-0.3
	1.260	2.395	2.40	0.005	0.2
	3.19	3.04	3.03	-0.01	-0.3
3.38	1.139	2.128	2.11	-0.018	-0.8
	5.09	2.551	2.55	-0.001	-0.04
	12.01	3.05	3.10	0.05	1.6

The values tabulated in columns I - III were taken directly from the original data given in Table 5. The values of  $C_p-C_v$  listed in column IV were read from the generalized correlation shown in Figure 4, corresponding to the reduced temperature and pressure conditions listed in columns I and II. These values are subject to the errors associated with averaging and interpolation. To determine the accuracy of the generalized correlation, the difference was taken between the generalized and calculated values of  $C_p-C_v$ . This difference, shown in column V, was then divided by the calculated value of  $C_p-C_v$ , and expressed as a percentage deviation in column VI.

The same procedure was followed for the other four gases, providing a sampling of points which covers the entire range of temperature and pressure included in the correlation. This information is presented in detail in Table 14. The large number of points sampled, makes it possible to accurately estimate the deviation of the generalized correlation from the data on which it was based.

### Comparison of Generalized Correlation with Correlation by Edmister:

Edmister has presented a generalized correlation for  $C_p-C_v$ , in graphical form, which partially covers the range submitted for this correlation (2). Specifically, the range common to both correlations include the reduced temperature range of  $T_r = 1.0$  to  $T_r = 2.5$  and the reduced pressure range of  $p_r = 0.2$  to  $p_r = 4.0$ . Edmister's correlation was compared with this correlation using the original  $C_p-C_v$  data as a reference. Values of  $C_p-C_v$  were read from Edmister's correlation corresponding to

temperature and pressure conditions based on the original data presented in Tables 3-7. The sampling method described earlier was used to cover the range common to both correlations. Percentage deviations were calculated for each point sampled. These values are presented in detail in Table 14.

### Comparison of Generalized Correlation with Data for Nitrogen and Carbon Monoxide:

Deming and Shupe have calculated values for  $C_p-C_v$ from very accurate p-V-T data obtained by Bartlett and co-workers for nitrogen and carbon monoxide  $(\frac{4}{5})(\frac{17}{12})$ . The range covered for nitrogen extends from  $-70^{\circ}$ C. to  $600^{\circ}$ C. and up to 1200 atmospheres pressure. For carbon monoxide, the range covered extends from  $-70^{\circ}$ C. to  $400^{\circ}$ C. and also up to 1200 atmospheres.

The generalized correlation prepared as a result of this work was used to estimate values of  $C_p-C_v$  for nitrogen and carbon monoxide over a large range of temperature and pressure. The sampling method used was similar to the one described earlier. For each gas, two extremes and a mean temperature were selected, and then, for each temperature, two extremes and a mean pressure were chosen. At each of these points, values of  $C_p-C_v$ were read from Figure 4 and compared with the values reported by Deming and Shupe. The purpose in making this comparison was to find out whether the generalized correlation can predict with reasonable accuracy values for  $C_p-C_v$  for non-polar and slightly polar gases in addition to hydrocarbons.

A comparison was also made using Edmister's correlation where temperature and pressure conditions permitted the use of this correlation. The results of these comparisons are shown in Tables 15 and 16 for nitrogen and carbon monoxide, respectively.

#### DISCUSSION OF RESULTS

#### General:

Since there is very little actual data at high pressure for  $C_p$  and almost none for  $C_v$ , it is extremely difficult to compare and evaluate the generalized correlation prepared as a result of this work. However, the correlation can be compared with the original data on which it was based and with Edmister's generalized correlation for  $C_p-C_v$ . Final evaluation of this work must wait until additional experimental data are obtained.

### The Generalized Correlation:

The generalized correlation prepared as a result of this work is presented in Table 13 and is shown graphically in Figure 4.  $C_p$ - $C_V$ , in molal units, is plotted as a function of reduced pressure, with parameters of reduced temperature. Beduced pressure varies between  $p_r = 0.2$  to  $p_r = 15.0$ . Eighteen parameters of reduced temperatures are presented ranging from  $T_r = 1.0$  to  $T_r = 5.5$ .

For an ideal gas  $C_p^*-C_v^* = R$ . For an actual gas  $C_p-C_v$ is generally larger; its value depending on the particular gas in question and its temperature and pressure. As one might expect,  $C_p-C_v$  approaches R for all temperatures as the pressure approaches zero. In general, at any particular pressure, the value for  $C_p-C_v$  increases with decreasing temperature.

Edmister has also presented a generalized correlation for  $C_p-C_v$  (2). The table below compares the range of variables presented in this correlation with that prepared by Edmister.

	Edmister	Bleich
p <sub>r</sub>	0.04 - 4.0	0.2 - 15.0
T <sub>r</sub>	0.8 - 2.5	1.0 - 5.5

### Comparison of Generalized Correlations with Original Data:

Table 14 contains a representative sampling of data points for each of the five gases studied. The original calculated values of  $C_p-C_v$ , for each of these points, are compared with values read from Figure 4 and Edmister's generalized correlation. The percentage deviation for each point is also listed in Table 14. As mentioned earlier, the values of  $C_p-C_v$  read from the generalized correlations are subject to the errors associated with averaging and interpolation.

The data in Table 14 shows that the deviation of the generalized correlation from the original data ranges from -8.1% to +4.6% for the 68 points checked. The higher deviations occur in the region of very high reduced pressure. The average deviation for the 68 points investigated amounts to only  $\pm 0.93\%$ . Edmister's correlation has been compared in a similar manner using 44 data points common to both correlations. The table below compares the deviation of the two correlations from the original data for the five gases studied.

	Edmister	Bleich
Number of Data Points Compared	44	44
Range of Deviations, %	-8.8 to +3.5	-0.9 to +3.2
Average Percentage Deviation	±2.36	±0.56

Edmister's correlation shows over four times the average deviation as that obtained for this correlation. This comparison serves to emphasize that whenever data for a specific gas are unavailable, this correlation should be used in preference to Edmister's generalized correlation.

### Comparison of Generalized Correlation with Data for Nitrogen and Carbon Monoxide:

 $C_p-C_v$  data, for nitrogen and carbon monoxide, reported by Deming and Shupe have been compared with corresponding values read from the generalized correlation shown in Figure 4 (4)(5). The individual data points used in this comparison are listed in Tables15 and 16 for nitrogen and carbon monoxide, respectively. The deviations found in comparing the generalized correlation with the original data are shown below:

	Nitrogen	<u>Carbon Monoxide</u>
Number of Data Points Compare	a 9	9
Range of Deviations, %	-2.9 to +14.6	-3.5 to +19.6
Average Percentage Deviation	±4.93	±6.40

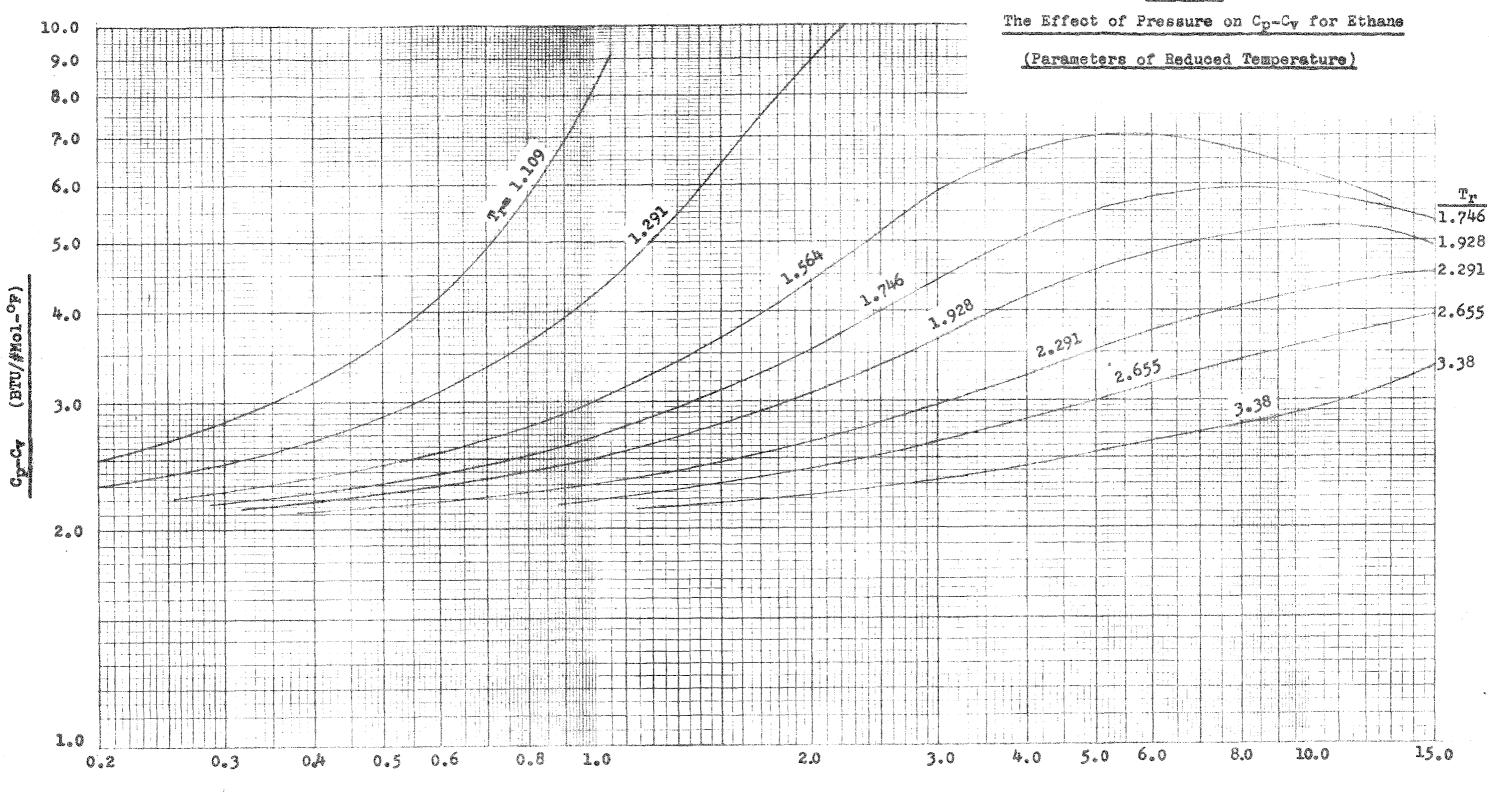
The agreement shown in this table is close enough to indicate that Figure 4 is suitable for use as a generalized correlation for non-polar and slightly polar gases in addition to hydrocarbons.

#### CONCLUSIONS AND RECOMMENDATIONS

A generalized correlation for  $C_p-C_v$  has been prepared as a result of this work which is believed to be more accurate than the correlation previously published by Edmister (2). The present correlation has been prepared by averaging values of  $C_p-C_v$ , covering a wide range of temperature and pressure, for five hydrocarbons. The gases studied were methane, ethylene, ethane, propane, and n-butane. The values of  $C_p-C_v$  were calculated from the Benedict - Webb - Rubin Equation of State. This equation is considered to be the most accurate equation of state developed to date.

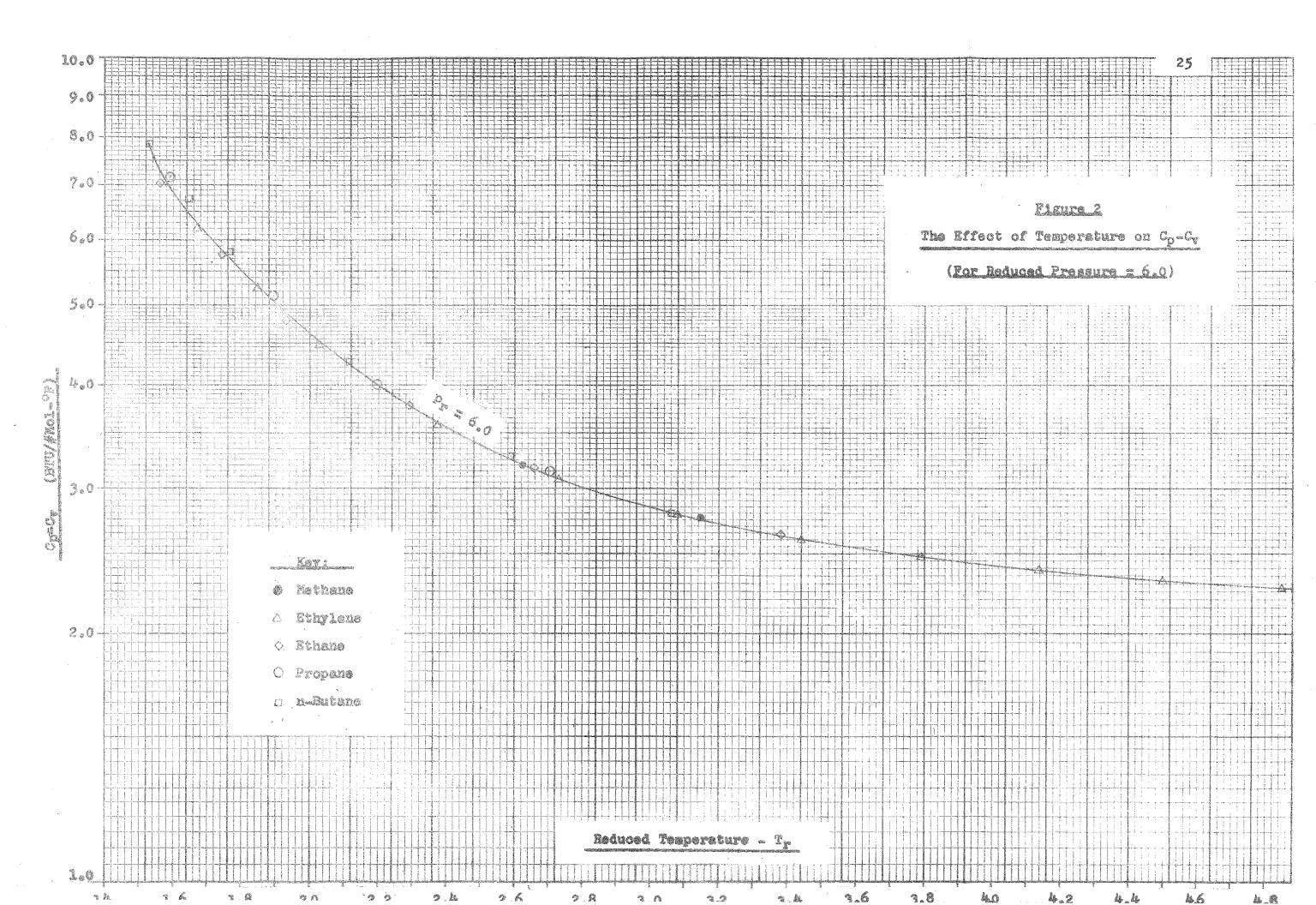
The generalized correlation prepared in this study has been compared with the original data on which it was based and with the generalized correlation presented by Edmister (2). The correlation was also used to predict values of  $C_p-C_v$  for nitrogen and carbon monoxide. The values obtained were compared with the data of Deming and Shupe (4)(5). The results of these comparisons indicate that this correlation is suitable for non-polar and slightly polar gases as well as hydrocarbons.

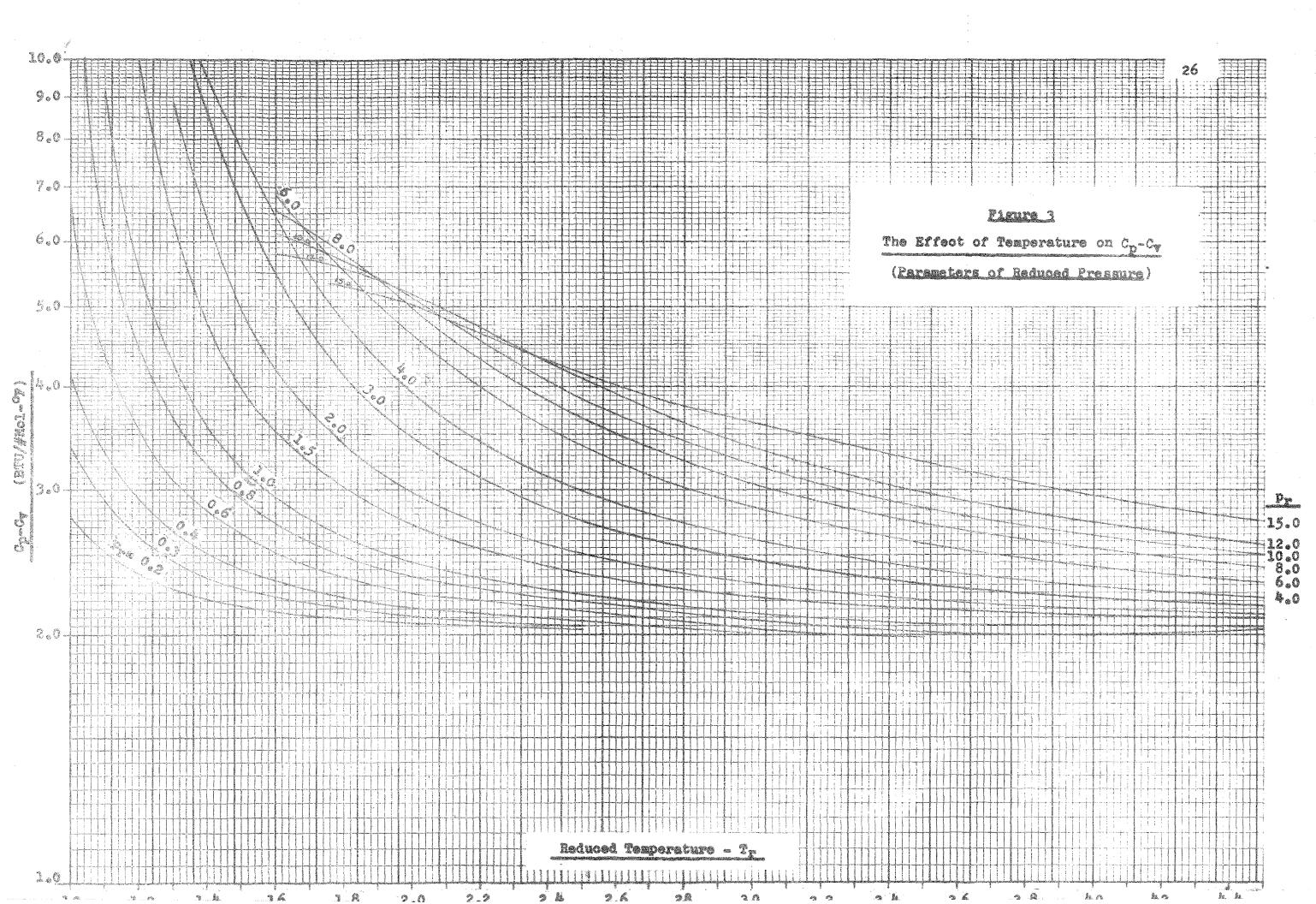
It is recommended that this correlation be used to obtain values for  $C_{p}-C_{v}$  in preference to other means whenever experimental data are unavailable or whenever time does not permit calculation of the desired value from the Benedict - Webb - Rubin Equation of State. APPENDIX

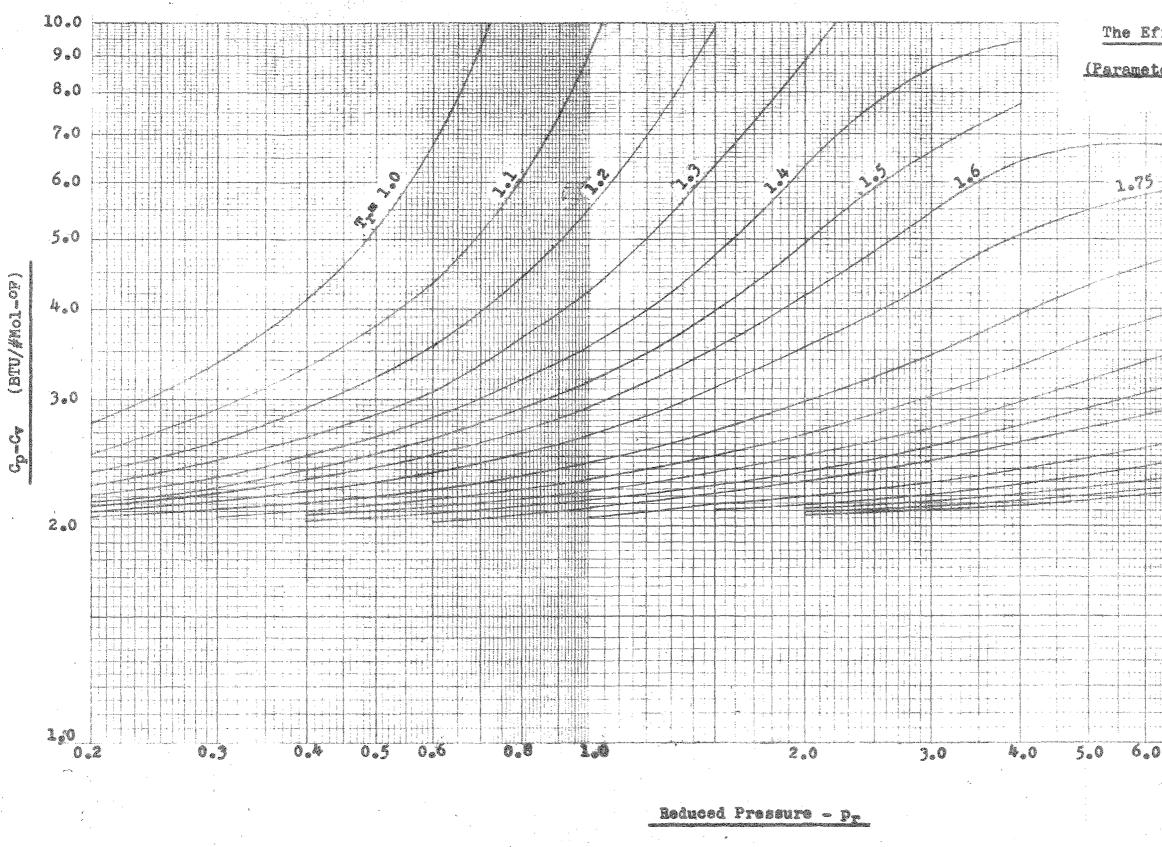


Beduced Pressure - pr

### Figure 1







#### Fisure 4

# The Effect of Pressure on Cp-Cy

#### (Parameters of Reduced Temperature)

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Benedict - Webb - Rubin Equation of State:  $P = RTV^{-1} + (B_{0}RT - A_{0} - C_{0}T^{-2})V^{-2} + (bRT - a)V^{-3}$   $+ a \propto V^{-6} + cV^{-3}(1 + \chi V^{-2})T^{-2}e^{-(\chi V^{-2})}$ where: P = Absolute Pressure (psia) R = Gas Law Constant; 10.7335 (psia)(ft<sup>3</sup>)/(#-mol)(°R) T = Absolute Temperature; <sup>O</sup>R (459.69 - <sup>O</sup>F) V = Molal Volume (ft<sup>3</sup>/#-mol) e = 2.71828

Benedict - Webb - Rubin Constants (psia. ft3, #-mol. OR):

	Methane	Ethvlene	Ethane	Propane	n-Butane
Bo	0.682401	0.891980	1.00554	1.55884	2.20329
Aox10 <sup>-4</sup>	0.699525	1.25936	1.56707	2.59154	3.85874
Cox10-9	0.275763	1.60228	2.19427	6.20993	10.3847
Ъ	0.867325	2.20678	2.85393	5.77355	10.8890
ax10 <sup>-4</sup>	0.298412	1.56455	2.08502	5.72480	11.7047
8	0.511172	0.731661	1.00044	2.49577	4.41496
c x 10 <sup>-9</sup>	0.498106	4.13360	6.41314	25.2478	55.9777
8	1.53961	2.36844	3.02790	5.64524	8.72447

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Molecular Weights and Critical Properties of Hydrocarbons	Molecular	Weights an	d Critica)	L Properties	of Hydrocarbo	n <u>s</u>
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	Molecular Formula	Molecular <u>Weight</u>	Critical Temperature To (OR)	Critical Pressure D (psia)
Methane	CH4	16.042	343.3	673.1
Ethylene	C <sub>2</sub> H <sub>4</sub>	28.052	509.51	742.1
Ethane	C <sub>2</sub> H <sub>6</sub>	30.068	549.77	708.3
Propane	C <sub>3</sub> H <sub>8</sub>	44.094	665.95	617.4
n-Butane	C4H10	58.120	765.31	550.7

	Differe	nce in Heat Ca	pacitie	<u>s for Me</u>	thane
t	p	C <sub>p</sub> +C <sub>▼</sub>	T r	p <b>r</b>	<sup>C</sup> p <b>-</b> C <sub>▼</sub>
(OP)		$(Btu/#Mol_OF)$	-		(Btu/#Mol_OF)
80.3	500 750	2.675 3.11	1.573	0.743 1.114	2.675 3.11
170.3	500 750 1000 1500	2.400 2.667 2.947 3.48	1.835	0.743 1.114 1.486 2.229	2.400 2.667 2.947 3.48
260.3	500 750 1000 1500 2000 3000	2.283 2.448 2.612 2.948 3.26 3.79	2.097	0.743 1.114 1.486 2.229 2.971 4.46	2.283 2.448 2.612 2.948 3.26 3.79
440.3	500 750 1000 1500 2000 3000 5000 5000 6000 7000 8000	2.156 2.248 2.334 2.519 2.671 2.956 3.19 3.37 3.51 3.61 3.68	2.622	0.743 1.114 1.486 2.229 2.971 4.46 5.94 7.43 8.91 10.40 11.89	2.156 2.248 2.334 2.519 2.671 2.956 3.19 3.37 3.51 3.61 3.68

Difference in Heat Capacities for Methane

#### Difference in Heat Capacities for Methane

t	p	°p <b>−°</b> ▼	T <sub>r</sub>	p <sub>r</sub>	C <sub>p</sub> +C <sub>v</sub>
(°F)	(DSIA)	(Btu/#Mol-OF)		anna hir tir cine an sui	(Btu/#Mol_OP)
620.3	500 750 1000 1500 2000	2.103 2.157 2.211 2.320 2.425	3.15	0.743 1.114 1.486 2.229 2.971	2.103 2.157 2.211 2.320 2.425
	2000 3000 5000 6000 7000	2.608 2.760 2.890 2.998 3.09		4.46 5.94 7.43 8.91 10.40	2.608 2.760 2.890 2.998 3.09
	8000 9000 10000	3.17 3.24 3.30		11.89 13.37 14.86	3.17 3.24 3.30
980.3	6000 7000 8000 9000 10000	2.536 2.601 2.655 2.707 2.748	4.19	8.91 10.40 11.89 13.37 14.86	2.536 2.601 2.655 2.707 2.748
1340.3	500 1000 2000 3000 4000 5000 5000 5000 7000 8000 9000 10000	2.025 2.063 2.132 2.239 2.239 2.286 2.331 2.377 2.408 2.453 2.484	5.24	0.743 1.486 2.971 4.46 5.94 7.43 8.91 10.40 11.89 13.37 14.86	2.025 2.063 2.132 2.193 2.239 2.286 2.331 2.377 2.408 2.453 2.484

Differe)	<u>nce in Heat Ca</u>	adacities	for sth	vlene
p	°p−°▼	$\mathbf{T}_{\mathbf{r}}$	p <sub>r</sub>	c <sub>p</sub> -c <sub>v</sub>
(ps1a)	(Liter-Atm) (Gm-Mol-K)	· And a first and a second		( <u>Btu</u> ) (#Mol_ <sup>O</sup> F)
624.8 616.7 587.7 553.9 458.1 346.2 276.0 151.0 63.65	4.064 2.307 1.072 0.7028 0.4015 0.2315 0.1778 0.1203 0.09553	0.965	0.842 0.831 0.792 0.746 0.617 0.467 0.372 0.2035 0.0858	98.4 55.8 25.94 17.01 9.72 5.60 4.30 2.912 2.312
1023. 941.6 915.0 825.8 749.8 585.4 424.9 332.6 177.2 73.65	0.8246 0.6779 0.5805 0.4388 0.3564 0.2369 0.1684 0.1417 0.1085 0.09191	1.106	1.379 1.269 1.233 1.113 1.010 0.789 0.573 0.448 0.2388 0.0992	19.96 16.41 14.05 10.62 8.63 5.73 4.08 3.43 2.626 2.224
$1595. \\ 1422. \\ 1342. \\ 1165. \\ 1030. \\ 766.8 \\ 538.2 \\ 414.5 \\ 215.8 \\ 88.51$	0.3626 0.3270 0.2996 0.2546 0.2239 0.1709 0.1361 0.1207 0.09994 0.08889	1.318	2.149 1.916 1.808 1.570 1.388 1.033 0.725 0.559 0.2908 0.1193	8.78 7.91 7.25 6.16 5.42 4.14 3.29 2.921 2.419 2.151
	p (ps1a) 624.8 616.7 587.7 553.9 458.1 346.2 276.0 151.0 63.65 1023. 941.6 915.0 825.8 749.8 585.4 424.9 332.6 177.2 73.65 1595. 1422. 1342. 1342. 1342. 1342. 1342. 1342. 1345. 1030. 766.8 538.2 414.5 215.8	p $C_p-C_v$ (DS18)(Liter-Atm) (Gm-Mol-K)624.84.064616.72.307587.71.072553.90.7028458.10.4015346.20.2315276.00.1778151.00.120363.650.095531023.0.8246941.60.6779915.00.5805825.80.4388749.80.3564585.40.2369424.90.1684332.60.1417177.20.108573.650.091911595.0.36261422.0.32701342.0.29961165.0.25461030.0.2239766.80.1709538.20.1361414.50.1207215.80.09994	p $C_p-C_v$ $T_r$ (DS18)( $Gm-Mol-K$ )(DS18)( $Gm-Mol-K$ )624.84.0640.965616.72.307587.71.072553.90.7028458.10.4015346.20.2315276.00.1778151.00.120363.650.09553	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

Difference in Heat Capacities for Ethylene

	Differen	ice in Heat Ca	apacitie	s for Eth	vlene
t	р	Cp-Cv	T <sub>r</sub>	p <sub>r</sub>	°p-°v
(°F)	(psia)	(Liter-Atm) (Gm-Mol- <sup>O</sup> K)	-	and a straight and a straight a	$\left(\frac{Btu}{\#Mol-{}^{o}F}\right)$
302	2061. 1810. 1688. 1438. 1255. 913.5 630.1 481.2 247.6 100.8	0.2637 0.2429 0.2272 0.2004 0.1813 0.1469 0.1226 0.1115 0.09517 0.08549	1.495	2.777 2.439 2.275 1.938 1.691 1.231 0.849 0.648 0.334 0.1358	6.38 5.88 5.50 4.85 4.39 3.56 2.967 2.699 2.303 2.069
392	5953. 4063. 3423. 2809. 2523. 2193. 2029. 1707. 1469. 1058. 720.7 547.2 279.2 113.1	0.2547 0.2559 0.2460 0.2276 0.2156 0.2009 0.1902 0.1902 0.1714 0.1577 0.1327 0.1327 0.1143 0.1056 0.09337 0.08646	1.672	8.02 5.48 4.61 3.79 3.40 2.955 2.734 2.300 1.980 1.980 1.426 0.971 0.737 0.376 0.1524	6.16 6.19 5.95 5.51 5.22 4.86 4.60 4.15 3.82 3.21 2.766 2.556 2.260 2.093

	Differen	ce in Heat Ca	paciti	es for Et	<u>hvlene</u>
t	р	C <sub>p</sub> −C <sub>▼</sub>	T <sub>r</sub>	p <sub>r</sub>	с <sub>р</sub> -с <sub>v</sub>
(°F)	(psia)	(Liter-Atm) (Gm-Mol- <sup>o</sup> K)	nerveden and die besteller state	un mart af an ar an ar	$\frac{(\underline{Btu})}{(\#Mol-{}^{\circ}F)}$
482	7375. 4952. 4127. 3343. 2982. 2571. 2366. 1973. 1696. 1200. 810.5 612.7 310.6 125.4	0.2251 0.2210 0.2119 0.1968 0.1874 0.1759 0.1679 0.1535 0.1430 0.1234 0.1088 0.1017 0.09155 0.08577	1.848	9.94 6.67 5.56 4.50 4.02 3.46 3.19 2.659 2.285 1.617 1.092 0.826 0.419 0.1690	5.45 5.35 5.13 4.76 4.54 4.26 4.06 3.72 3.46 2.987 2.633 2.461 2.216 2.076
572	8805. 5843. 4832. 3876. 3438. 2947. 2701. 2236. 1913. 1341. 899.7 677.9 341.9 137.6	0.2052 0.1983 0.1897 0.1768 0.1690 0.1595 0.1531 0.1415 0.1329 0.1170 0.1048 0.09885 0.09024 0.08587	2.025	11.86 7.87 6.51 5.22 4.63 3.97 3.64 3.01 2.578 1.807 1.212 0.913 0.461 0.1854	4.97 4.80 4.59 4.28 4.09 3.86 3.71 3.42 3.22 2.832 2.536 2.392 2.184 2.078

	Differe	nce in Heat (	apaciti	es for Eth	vlene
t	P	с <sub>р</sub> -с <sub>v</sub>	Tr	pr	cp-cv
<u>(°F)</u>	(psia)	( <u>Liter_Atm</u> ) ( <u>Gm-Mol_<sup>o</sup>K</u> )			( <u>Btu</u> ) (#Mol-°F)
752	7629 6242 4938 4347 3694 3367 2760 2343 1622 1077 807.6 404.4 162.1	0.1703 0.1626 0.1523 0.1464 0.1393 0.1347 0.1263 0.1197 0.1086 0.09953 0.09505 0.08845 0.08459	2.378	10.28 8.41 6.65 5.86 4.98 4.54 3.72 3.16 2.186 1.451 1.088 0.545 0.2184	4.12 3.94 3.69 3.54 3.37 3.26 3.06 2.897 2.628 2.409 2.300 2.141 2.047
932	9420 7507 5997 5254 4438 4029 3280 2772 1901 1254 936.8 466.7 186.5	0.1538 0.1468 0.1380 0.1332 0.1274 0.1239 0.1179 0.1124 0.1034 0.09622 0.09264 0.08698 0.08408	2.731	12.69 10.12 8.08 7.08 5.98 5.43 4.42 3.74 2.562 1.690 1.262 0.629 0.2513	3.72 3.55 3.34 3.22 3.08 2.999 2.853 2.720 2.502 2.329 2.242 2.105 2.035

	Differe	nce in Heat C	apaciti	es for Eth	vlene
t	р	Cp-Cv	Tr	Pr	Cp-Cv
(°F)	(psia)	(Liter_Atm) (Gm_Mol_ <sup>O</sup> K)	which are and the play	authaidheistan an Annaiche	( <u>Btu</u> ) (#Mol_ <sup>o</sup> F)
1112	9061 7055 6158 5179 4689 3799 3198 2180 1430 1066 529.0 210.9	0.1364 0.1286 0.1245 0.1196 0.1167 0.1112 0.1073 0.09985 0.09396 0.09396 0.09098 0.08372 0.08384	3.08	12.21 9.51 8.30 6.98 6.32 5.12 4.31 2.938 1.927 1.436 0.713 0.2842	3.30 3.11 3.01 2.895 2.824 2.691 2.597 2.417 2.274 2.202 2.026 2.029
1292	10470 8112 7061 5919 5347 4316 3624 2457 1606 1195 591.2 235.4	0.1291 0.1221 0.1184 0.1141 0.1116 0.1070 0.1036 0.09731 0.09231 0.08298 0.08364	3.44	14.11 10.93 9.51 7.98 7.21 5.82 4.88 3.31 2.164 1.610 0.797 0.317	3.12 2.955 2.866 2.761 2.701 2.590 2.507 2.355 2.234 2.173 2.008 2.024
1472	9169 7964 6658 6007 4833 4049 2735 1782 1323 653.4 259.8	0.1172 0.1138 0.1100 0.1078 0.1037 0.1008 0.09539 0.09106 0.08885 0.08240 0.08344	3.79	12.36 10.73 8.97 8.09 6.51 5.46 3.69 2.401 1.783 0.880 0.350	2.836 2.754 2.662 2.609 2.510 2.440 2.309 2.204 2.150 1.994 2.019

Difference in Heat Capacities for Ethylene							
t	p	Cp-Cv	T <sub>r</sub>	Pr	Cp-Cv		
_(°F)_		(Liter-Atm) (Gm-Mol-°K)	-	ana porta de 18 e incomposito	( <u>Btu</u> ) (#Mol_OF)		
1652	10230 8866 7396 6665 5350 4474 3012 1957 1452 715.6 284.2	0.1134 0.1103 0.1068 0.1049 0.1013 0.09866 0.09388 0.09007 0.08812 0.08513 0.08330	4.14	13.79 11.95 9.97 8.98 7.21 6.03 4.06 2.637 1.957 0.964 0.383	2.745 2.669 2.585 2.539 2.452 2.388 2.272 2.180 2.133 2.060 2.016		
1832	9767 8134 7322 5866 4899 3289 2133 1580 777.8 308.6	0.1075 0.1043 0.1025 0.09926 0.09693 0.09267 0.08928 0.08753 0.08484 0.08322	4.50	13.16 10.96 9.87 7.90 6.60 4.43 2.874 2.129 1.048 0.416	2.602 2.524 2.481 2.402 2.346 2.243 2.161 2.118 2.053 2.014		
2012	10670 8872 7980 6382 5323 3566 2308 1709 839.9 333.0	0.1053 0.1022 0.1006 0.09762 0.09551 0.09170 0.08863 0.08704 0.08460 0.08310	4.85	14.38 11.96 10.75 9.60 7.17 4.81 3.11 2.303 1.132 0.449	2.548 2.473 2.435 2.363 2.312 2.219 2.145 2.107 2.047 2.011		

	Difference in Heat Capacities for Ethylene							
t	p	Cp-Cv	T <sub>r</sub>	p <sub>r</sub>	Cp-Cv			
(°F)	(osta)	(Liter-Atm) (Gm-Mol- <sup>O</sup> K)	etalkatuuraa etalaa		$\frac{(Btu)}{(\#Mol-^{OF})}$			
2192	11570 9609 8637 6898 5747 3842 2484 1837 902.1 357.4	0.1034 0.1006 0.09905 0.09627 0.09434 0.09084 0.08807 0.08664 0.08440 0.08302	5.20	15.59 12.95 11.64 9.30 7.74 5.18 3.35 2.475 1.216 0.482	2.502 2.435 2.397 2.330 2.283 2.199 2.131 2.097 2.043 2.009			
2372	12470 10350 9287 7413 6172 4119 2659 1966 964.2 381.8	0.1018 0.09912 0.09771 0.09513 0.09334 0.09014 0.08760 0.08628 0.08432 0.08295	5.56	16.80 13.95 12.51 9.99 8.32 5.55 3.58 2.649 1.299 0.514	2.464 2.399 2.365 2.302 2.259 2.182 2.120 2.088 2.039 2.008			

Difference in Heat Capacities for Ethane								
t	р	Cp-Cv	Tr	$p_{\mathbf{r}}$	Cp=Cv			
<u>(0</u> F)	(psia)	(Btu/#_°F)		alan di salah kacima na mangalini madangan	(Btu/#-Mol-OF)			
150	744.0 556.5 374.0 238.7 125.0	0.3028 0.1888 0.1262 0.09814 0.08079	1.109	1.050 0.786 0.528 0.337 0.1765	9.10 5.68 3.79 2.951 2.429			
250	1676 1232 989.2 712.3 456.8 285.8 147.5	0.3544 0.2562 0.1964 0.1422 0.1066 0.08860 0.07670	1.291	2.366 1.739 1.397 1.006 0.645 0.404 0.2082	10.66 7.70 5.91 4.28 3.21 2.664 2.306			
400	9154 7016 5437 4178 3137 2574 1745 1344 929.1 577.6 355.0 180.9	0.1885 0.2078 0.2241 0.2334 0.2282 0.2137 0.1697 0.1417 0.1136 0.09272 0.08134 0.07344	1.564	12.92 9.91 7.68 5.90 4.43 3.63 2.464 1.898 1.312 0.815 0.501 0.2554	5.76 6.25 6.74 7.02 6.86 6.43 5.10 4.26 3.42 2.788 2.446 2.208			

TABLE 5

	Difference in Heat Capacities for Ethane								
t	р	°p <sup>-°</sup> v	$^{\mathrm{T}}\mathbf{r}$	p <sub>r</sub>	°p⁺°v				
( <b>0</b> F)	(psia)	(Btu/#_°F)		un alifer de culture de activités	(Btu/#Mol- <sup>o</sup> F)				
500	11757 9070 7018 5337 3929 3170 2081 1575 1071 657.0 400.7 203.0	0.07856	1.746	16.60 12.81 9.91 7.53 5.55 4.48 2.938 2.224 1.512 0.928 0.566 0.2866	5.16 5.54 5.82 5.93 5.69 5.33 4.36 3.75 3.12 2.635 2.362 2.169				
600	10447 8611 7395 6505 4722 3764 2414 1211 735.7 446.1 225.1	0.07662	1.928	14.75 12.16 10.44 9.18 6.67 5.31 3.41 1.710 1.039 0.630 0.318	4.92 5.23 5.26 5.23 4.98 4.67 3.90 2.922 2.529 2.304 2.142				

Difference in Heat Capacities for Ethane								
t	р	$C_{\mathbf{p}} - C_{\mathbf{v}}$	$\mathbf{T}_{\mathbf{r}}$	p <sub>r</sub>	°p-°v			
<u>(°F)</u>	(psia)	(Btu/#_ <sup>0</sup> F)		ana ala ana ana ana ana ana ana ana ana	(Btu/#Mol_OF)			
800	11821 8855 4951 3075 2259 1489 892.3 536.7 269.2	0.1506 0.1474 0.1302 0.1116 0.1010 0.08925 0.07965 0.07410 0.07007	2.291	16.69 12.50 6.99 4.34 3.19 2.102 1.260 0.758 0.380	4.53 4.43 3.91 3.36 3.04 2.684 2.395 2.228 2.107			
1000	11211 6136 3732 2710 1766 1319 1048 626.9	0.1323 0.1163 0.1015 0.09312 0.08410 0.07968 0.07694 0.07180	2.655	15.83 8.66 5.27 3.83 2.493 1.862 1.480 0.885	3.98 3.50 3.05 2.800 2.529 2.396 2.313 2.159			
1400	14262 8504 5041 3608 2323 1359 806.9	0.1340 0.1014 0.09057 0.08483 0.07882 0.07344 0.07076	3.38	20.14 12.01 7.12 5.09 3.28 1.919 1.139	4.03 3.05 2.723 2.551 2.370 2.208 2.128			

	Difference in Heat Capacities for Propane							
t	p	Cp-Cv	Tr	p <sub>r</sub>	c <sub>p</sub> -c <sub>v</sub>			
( <sup>0</sup> F)	(ps1a)	(Liter_Atm) (Gm-Mol- <sup>O</sup> K)	water the state of	-	$\frac{(Btu)}{(\#-Mol^{\circ}F)}$			
200	43.07 298.3 338.5 442.0	0.09252 0.2136 0.2529 0.5277	0.991	0.0698 0.483 0.548 0.716	2.239 5.17 6.12 12.77			
400	112.1 505.7 613.0 778.1 900.2 1070 1539 2701	0.09402 0.1550 0.1785 0.2222 0.2605 0.3210 0.4663 0.4921	1.291	0.1816 0.819 0.993 1.260 1.458 1.733 2.493 4.37	2.275 3.75 4.32 5.38 6.30 7.77 11.29 11.91			
500	207.4 585.5 1085 1697 2543 3000	0.09842 0.1375 0.2086 0.3291 0.3592 0.3599	1.441	0.336 0.948 1.757 2.749 4.12 4.86	2.382 3.33 5.05 7.96 8.69 8.71			
600	231.0 664.1 1267 2058 3213 4939	0.09559 0.1264 0.1793 0.2456 0.2914 0.2977	1.591	0.374 1.076 2.052 3.33 5.20 8.00	2.313 3.06 4.34 5.94 7.05 7.20			

Difference in Heat Capacities for Propane								
t	р	C <sub>p</sub> -C <sub>v</sub>	<sup>T</sup> r	p <sub>r</sub>	Cp-Cv			
(°F)	(psia)	(Liter-Atm) (Gm-Mol- <sup>O</sup> K)	4 <u>402445.444.4444</u>		$(\underline{Btu}) \\ (\#-Mol-^{\sigma}F)$			
800	276.4 550.2 818.9 1162 2769 4565 5554 7233	0.09194 0.1024 0.1135 0.1282 0.1900 0.2242 0.2310 0.2359	1.892	0.448 0.891 1.326 1.882 4.48 7.39 9.00 11.72	2.225 2.478 2.747 3.10 4.60 5.43 5.59 5.71			
1000	97.64 486.1 973.4 1394 1976 3484 4364 5925 6958 8465 9554	0.08436 0.09391 0.1063 0.1172 0.1317 0.1627 0.1756 0.1909 0.1964 0.2019 0.2029	2 <b>.19</b> 2	0.1581 0.787 1.577 2.258 3.20 5.64 7.07 9.60 11.27 13.71 15.47	2.042 2.273 2.573 2.836 3.19 3.94 4.25 4.62 4.62 4.75 4.89 4.91			
1340	120.7 491.5 1230 1785 2569 4689 8248	0.08377 0.09670 0.09940 0.1069 0.1169 0.1386 0.1543	2.702	0.1955 0.796 1.992 2.891 4.16 7.59 13.36	2.027 2.340 2.406 2.587 2.829 3.35 3.73			

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DITIETENCE IN NEAR VADAGICIES IUT ASDUCANE							
t	р	$c_p - c_v$	Tr	p <sub>r</sub>	Cp-Cv		
<u>(°F)</u>	(psia)	(Liter-Atm) (Gm-Mol- <sup>O</sup> K)			( <u>Btu</u> ) (#-Mol- <sup>o</sup> F)		
350.4	896.1 610.9 492.5 407.0 237.0 102.6	1.570 0.8406 0.4085 0.2796 0.1550 0.1067	1.059	1.627 1.109 0.894 0.739 0.429 0.1863	38.0 20.34 9.89 6.77 3.75 2.582		
440.4	801.0 637.0 605.9 486.6 270.5 115.5	0.4598 0.3078 0.2854 0.2159 0.1364 0.1012	1.176	1.455 1.157 1.100 0.884 0.491 0.2097	11.13 7.45 6.91 5.23 3.30 2.449		
485.4	1296 1153 893.9 813.1 661.4 525.4 287.8 121.9	0.5802 0.5320 0.3725 0.3317 0.2377 0.1965 0.1300 0.09923	1.235	2.353 2.094 1.623 1.476 1.201 0.954 0.523 0.2214	14.04 12.88 9.02 8.03 5.75 4.76 3.15 2.402		
530.4	1764 1482 1305 985.8 715.8 563.7 305.0	0.4979 0.4795 0.4420 0.3285 0.2271 0.1817 0.1248	1.294	3.20 2.691 2.370 1.790 1.300 1.024 0.554	12.05 11.60 10.70 7.95 5.50 4.40 3.02		

#### Difference in Heat Capacities for n-Butane

#### Difference in Heat Capacities for n-Butane $C_{p}-C_{v}$ Tr pr t Cp-Cv p (Liter-Atm) Btu (°F) (Gm-Mol-OK)#-Mol-P (psia) 3.66 575.4 2013 1669 10.43 9.98 0.4308 1.353 0.4125 3.03 2.669 1470 0.3815 9.23 1.956 7.04 1077 0.2910 769.7 0.2084 1.398 5.04 601.6 4.12 0.1701 1.092 322.0 0.1206 0.585 2.919 620.4 5.56 4.57 4.11 3063 1.411 0.3753 9.08 2514 0.3843 9.30 2263 0.3830 9.27 3.37 2.905 2.119 1856 0.3648 8.83 0.3381 0.2631 8.18 1600 6.37 1167 3.89 0.1607 639.1 1,161 442.8 0.804 0.1307 2.834 0.1171 0.615 338.9 647.4 4.87 2681 0.3623 1.447 8.77 2413 1968 8.71 8.28 0.3600 4.38 0.3423 3.57 1688 7.69 0.3176 3.07 0.2495 2.217 1221 1.553 855.2 4.52 0.1868 3.77 0.1559

	Differen	nce in Heat Ca	pacities	s for n-Bi	itane
t	p	Cp−C¥	Tr	$\mathbf{p_r}$	Cp-Cv
<u>(°F)</u>	<u>(ps1a)</u>	( <u>Liter-Atm</u> ) ( <u>Gm-Mol-<sup>O</sup>K</u> )			$\frac{(Btu)}{(\#-Mol-^{O}F)}$
665.4	2797 2513 2043 1748 1257 876.1 676.4 355.8 148.1	0.3495 0.3468 0.3292 0.3056 0.2415 0.1819 0.1530 0.1141 0.09399	1.470	5.08 4.56 3.71 3.17 2.283 1.591 1.228 0.646 0.2689	8.46 8.39 7.97 7.40 5.84 4.40 3.70 2.761 2.275
710.4	3814 3088 2764 2230 1895 1346 928.7 713.4 372.5	0.3203 0.3223 0.3187 0.3016 0.2803 0.2244 0.1723 0.1467 0.1115	1.529	6.93 5.61 5.02 4.05 3.44 2.444 1.686 1.295 0.676	7.75 7.80 7.71 7.30 6.78 5.43 4.17 3.55 2.699
800.4	4574 3269 2603 2190 1523 786.9 405.8 166.1	0.2943 0.2779 0.2616 0.2436 0.1944 0.1367 0.1074 0.09168	1.647	8.31 5.94 4.73 3.98 2.766 1.429 0.737 0.302	7.12 6.73 6.33 5.90 4.70 3.31 2.599 2.219

Difference in Heat Capacities for n-Butane

Difference in Heat Capacities for n-Butane								
t	P	cp-cv	Tr	p <b>r</b>	Cp-Cv			
<u>(°F)</u>	(osia)	( <u>Liter-Atm</u> ) ( <u>Gm-Mol-<sup>O</sup>K</u> )			$\frac{(Btu)}{(\#-Mol-^{o}F)}$			
890.4	5340 3776 2977 1698 859.7 439.0 178.6	0.2589 0.2496 0.2313 0.1769 0.1293 0.1043 0.09056	1.764	9,70 6.86 5.41 3.08 1.561 0.797 0.324	6.27 6.04 5.60 4.28 3.13 2.524 2.192			
1160.4	7660 5305 4097 2220 1076 537.6 216.0	0.2132 0.2005 0.1870 0.1496 0.1154 0.09818 0.08731	2.117	13.91 9.63 7.44 4.03 1.954 0.976 0.392	5.16 4.85 4.53 3.62 2.793 2.376 2.113			
1520.4	7574 5592 2908 1361 672.6	0.1690 0.1572 0.1294 0.1059 0.09381	2.587	13.75 10.15 5.28 2.471 1.221	4.09 3.80 3.13 2.563 2.270			
1880.4	9408 7087 3593 1644 798.2	0.1520 0.1413 0.1185 0.1005 0.09129	3.06	17.08 12.87 6.52 2.985 1.449	3.68 3.42 2.868 2.432 2.209			

				- T <sub>r</sub>	State Show and Spinster and spin	-	
	1.573	1.835	2.097	-r <u>2.622</u>	3.15	4.19	5.24
15 12 10				3.59	3.18 3.06	2.66 2.58	2.48 2.41 2.36
8 6 4			3.62	3.43 3.20 2.87	2.92 2.77 2.55		2.30 2.24 2.17
3 2 1.5		3.29 2.95	3.27 2.84 2.63	2.68 2.46 2.35	2.43 2.29 2.23		2.13 2.08 2.06
1.0 0.8 0.6	3.00 2.75	2.60 2.45	2.40 2.30	2.23 2.18	2.15 2.11		2.03 2.025
0.4 0.3 0.2					·		

TABLE 8

 $C_p-C_v$  Data for Methane (Parameters of  $p_r$ )

	Cp-Cv	Data for	Ethyle	ne (Para	neters of	( p <sub>r</sub> )
				<b>N</b>	-	
r	0.965	1.106	1.318	°r 1.495	1.672	1.848
15 12 10						5.45
8 6 4					6.16 6.20 5.70	5.40 5.24 4.53
3 2 1.5			8.25 5.87	4.97 4.01	4.88 3.85 3.30	3 <b>.95</b> 2.27 2.90
1.0 0.8 0.6	29 9.0	8.45 5.85 4.24	4.05 3.47 3.01	3.19 2.90 2.64	2.79 2.60 2.44	2.57 2.45 2.33
0.4 0.3 0.2	4.65 3.57 2.90	3.25 2.86 2.50	2.63 2.44 2.27	2.38 2.26 2.13	2.28 2.20 2.12	2.21 2.15 2.09

TABLE 9

					han all and the second	
<b></b>	2.025	2.378	<u>2.731</u>	3.08	3.44	3.79
15 12 10	4.97 4.92	4.10	3.69 3.53	3.29 3.15	3.02 2.90	2.83 2.71
8 6 4	4.81 4.48 3.87	3.88 3.58 3.14	3.33 3.08 2.78	2.99 2.80 2.57	2.76 2.60 2.41	2.60 2.48 2.33
3 2 1.5	3.42 2.94 2.69	2.86 2.57 2.43	2.59 2.40 2.29	2.44 2.28 2.21	2.32 2.20 2.15	2.26 2.17 2.10
1.0 0.8 0.6	2.43 2.33 2.23	2.28 2.22 2.16	2.18 2.13 2.10	2.10 2.06 2.01	2.06 2.01 1.99	2.01 1.98 1.98
0.4 0.3 0.2	2.15 2.10 2.07	2.10 2.06 2.04	2.06 2.04	2.00 2.02	2.00	2.00

TABLE 9 (Con't.)

 $C_p-C_v$  Data for Ethylene (Parameters of  $p_r$ 

	-				•
<u> </u>	4.14	4.50	<b>4</b> .85	5.20	5.56
15 12 10	2.67 2.59	2.57 2.49	2.48 2.40	2.48 2.41 2.36	2.44 2.36 2.30
8 6 4	2.50 2.39 2.26	2.41 2.32 2.22	2.34 2.27 2.20	2.30 2.23 2.15	2.25 2.20 2.13
3 2 1.5	2.20 2.14 2.10	2.17 2.12 2.09	2.15 2.10 2.08	2.12 2.08 2.05	2.10 2.06 2.05
1.0 0.8 0.6	2.07 2.04 2.02	2.05 2.03 2.01	2.04 2.02 2.01	2.02 2.01 2.00	2.03 2.02 2.01
0.4 0.3 0.2	2.01				

 $C_p-C_v$  Data for Ethylene (Parameters of  $p_r$ )

A 771	$\mathbf{n}\mathbf{r}$	7.7	3 A
- I M	BI	. N.	8.5
		a de la compañía de l	

$C_n - C_v$ Data for Ethan	ne (Parameters of $p_r$ )
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		Carthaig and State and State of State		T.				
p	1.109	1.291	1.564	1.746	1.928	2.291	2.655	3.38
15 12 10			5.83 6.22	5.31 5.65 5.81	5.23 5.24	4.50 4.40 4.29	3.92 3.76 3.60	3.35 3.04 2.90
8 6 4			6.69 7.01 6.67	5.90 5.77 5.10	5.13 4.80 4.17	4.08 3.77 3.27	3.42 3.18 2.82	2.78 2.64 2.44
3 2 1.5		8.95 6.50	5.88 4.40 3.69	4.41 3.52 3.10	3.65 3.09 2.80	2.97 2.64 2.48	2.64 2.44 2.32	2.34 2.225 2.17
1.0 0.8 0.6	8.60 5.81 4.19	4.25 3.61 3.10	3.01 2.77 2.56	2.68 2.53 2.38	2.50 2.39 2.28	2.31 2.25 2.19	2.20	
0.4 0.3 0.2	3.20 2.83 2.51	2.66 2.46 2.30	2.36 2.26	2.24 2.18	2.175	2.12		

				T			
	0.991	1.291	1.441	1.591	1.892	2.192	2.702
15 12 10					5.64	4•90 4•78 4•65	3.68 3.54
8 6 4		11.90	8.69	7.20 7.19 6.50	5.50 5.13 4.32	4.40 4.01 3.43	3.38 3.15 2.80
3 2 1.5		11.85 9.45 6.50	8.20 5.80 4.41	5.54 4.27 3.57	3.74 3.15 2.85	3.10 2.73 2.55	2.61 2.41 2.37
1.0 0.8 0.6	7.21	4.35 3.70 3.15	3.42 3.09 2.77	2.97 2.75 2.55	2.55 2.43 2.31	2.35 2.28 2.20	2.35 2.34 2.29
0.4 0.3 0.2	4.27 3.48 2.86	2.70 2.50 2.30	2.475	2.35		2.125 2.09 2.05	2.225 2.15 2.03

TABLE 11

	Cp-Cv	Data fo	r n-Buta	ne (Para	meters o	f p <sub>r</sub> )	
				- Tr			
	1.059	1.176	1.235	1.294	1.353	1.411	1.447
15 12 10							
8 6 4			1				
4						9.20	8.55
3 2 1.5	34.8		12.3 8.20	12.0 9.05 6.40	9.95 7.21 5.40	8.33 5.98 4.60	7•55 5•51 4•42
1.0 0.8 0.6	14.4 7.85 5.07	6.10 4.72 3.71	4.92 4.18 3.44	4.37 3.72 3.15	3.90 3.39 2.95	3.53 3.15 2.80	
0.4 0.3 0.2	3•59 3•07 2•63	3.00 2.80 2.43					

TABLE 12

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		مر و مر و المر و المر و مر و مر و المر و مر و		- T <sub>r</sub>			
	1.470	1.529	1.647	1.764	2.117	2.587	3.06
15 12 10					5.05 4.89	3.96 3.79	3.55 3.35 3.20
8 6 4	8.19	7.85 7.28	7.10 6.75 5.91	6 <b>.1</b> 9 5.82 4.89	4.63 4.27 3.61	3.58 3.28 2.90	3.02 2.80 2.56
3 2 1.5	7.17 5.27 4.21	6.23 4.66 3.87	5.00 3.90 3.39	4.23 3.50 3.09	3.26 2.82 2.60	2.69 2.46 2.34	2.45 2.30 2.22
1.0 0.8 0.6	3.29 2.97 2.69	3.15 2.87	2.88 2.67 2.47	2.69 2.53 2.38	2.39 2.30 2.21		
0.4 0.3 0.2	2.43 2.30		2.39 2.21	2.23	2.12		

TABLE 12 (Con't.)

 $C_p-C_v$  Data for n-Butane (Parameters of  $p_r$ )

# Generalized Correlation for $C_p-C_v$

# (Parameters of Reduced Pressure and Temperature)

_Pr_	1.0	1.1	1.2	_ <u>l.</u> 3	1.4	1.5	
15 12 10							
8 6 4				11.7	9.47	7.74	
3 2 1.5		21.6	9.85	11.6 8.85 6.31	8.66 6.32 4.77	6.66 4.94 3.98	
1.0 0.8 0.6	13.7 6.78	9.15 6.10 4.35	5.53 4.44 3.54	4 <b>.27</b> 3.66 3.08	3.56 3.20 2.835	3.18 2.915 2.65	
0.4 0.3 0.2	4.11 3.376 2.78	3.32 2.90 2.52	2.92 2.625 2.375	2.67 2.46 2.275	2.51 2.345 2.21	2.40 2.27 2.17	

# Generalized Correlation for $C_p-C_v$

#### (Parameters of Reduced Pressure and Temperature)

			T	and an electronic links (here the second		
	1.60	1.75	2.00	2.25	2.50	2.75
15 12 10	5.80 6.18	5.31 5.65 5.81	5.02 5.18 5.13	4.57 4.60 4.41	4.20 4.09 3.85	3.83 3.68 3.50
8 6 4	6.55 6.85 6.43	6.00 5.79 5.08	4.97 4.62 3.93	4.18 3.86 3.335	3.65 3.39 2.985	3.31 3.06 2.77
3 2 1.5	5.46 4.19 3.53	4.37 3.55 3.11	3.47 2.965 2.71	3.04 2.68 2.505	2.74 2.505 2.375	2.58 2.39 2.285
1.0 0.8 0.6	2.94 2.715 2.515	2.69 2.53 2.38	2.45 2.35 2.245	2.325 2.255 2.19	2.24 2.185 2.145	2.175 2.14 2.09
0.4	2.33 2.225 2.13	2.24 2.18 2.10	2.155 2.115 2.07	2.11 2.07 2.05	2.08 2.05 2.03	2.04 2.03

# Generalized Correlation for $C_p - C_v$

#### (Parameters of Reduced Pressure and Temperature)

r_	3.0	_3.5_	4.0	4.5	5.0	_5.5_
15	3.61	3.27	2.95	2.75	2.55	2.45
12	3.375	2.98	2.725	2.57	2.46	2.375
10	3.22	2.87	2.63	2.50	2.40	2.32
8	3.05	2.725	2.54	2.41	2.325	2.26
6	2.85	2.58	2.42	2.32	2.25	2.21
4	2.61	2.40	2.29	2.22	2.17	2.13
3	2.47	2.30	2.22	2.17	2.125	2.10
2	2.31	2.20	2.15	2.12	2.09	2.065
1.5	2.225	2.15	2.11	2.09	2.09	2.05
1.0	2.125	2.06	2.055	2.05	2.045	2.035
0.8	2.08	2.01	2.00	2.03	2.025	2.02
0.6	2.03	1.99	2.00	2.01	2.01	2.01
0.4 0.3 0.2	2.005 2.02	2.00	2.00			

#### Comparison of the Generalized Correlations of Bleich and Edmister with Original Data

#### METHANE

	,	$C_p - C_v$			Diff	erence	% Deviation	
<u> </u>	<b>p</b>	Calculated	Bleich	Edmister	Bleich	Edmister	Bleich	Edmister
1.573	0.743 1.114	2.675 3.11	2.70 3.12	2.69 3.11	0.025 0.01	0.015	0.9 0.3	0.6 0.0
1.835	0.743 1.486 2.229	2.400 2.947 3.48	2.42 2.95 3.50	2.48 2.95 3.40	0.02 0.003 0.02	0.08 0.003 -0.08	0.8 0.1 0.6	3.3 0.1 -2.3
2 <b>.</b> 09 <b>7</b>	0.743 1.486 2.971	2.283 2.612 3.26	2.28 2.62 3.28	2.33 2.69 3.30	-0.003 0.008 0.02	0.047 0.078 0.04	-0.1 0.3 0.6	2.1 3.0 1.2
2.622	0.743 4.46 11.89	2 <b>.156</b> 2.956 3.68	2.15 2.95 3.85	4 *	-0.006 -0.006 0.17		-0.3 -0.2 4.6	
4.19	8.91 11.89 14.86	2.536 2.655 2.748	2.53 2.66 2.85	<b>북</b> 중 북	-0.006 0.005 0.102		-0.2 0.2 3.7	

\* Outside of the limits of Edmister's correlation.

#### Comparison of the Generalized Correlations of Bleich and Edmister with Original Data

#### ETHYLENE

		<u> </u>	$p = C_{\rm V}$		Diff	Difference		% Deviation	
Tr	p_r	Calculated	Bleich	Edmister	Bleich	Edmister	Bleich	Edmister	
1.106	0.2388 0.789 1.010	2.626 5.73 8.63	2.65 5.80 8.70	2.62 5.60 8.50	0.024 0.07 0.07	-0.006 -0.13 -0.13	0.9 1.2 0.8	-0.2 -2.3 -1.5	
1.672	0.376 1.980 3.79	2.260 3.82 5.51	2.26 3.82 5.55	2.28 3.75 5.30	0.00 0.00 0.04	0.02 -0.07 -0.21	0.0 0.0 0.7	0.9 -1.8 -3.8	
2.378	0.545 2.186 3.72 4.54 10.28	2.141 2.628 3.06 3.26 4.12	2.14 2.63 3.06 3.27 4.14	2.20 2.72 3.15 *	-0.001 0.002 0.00 0.01 0.02	0.059 0.092 0.09	-0.05 0.1 0.0 0.3 0.5	2.8 3.5 3.0	
4.85	2.303 7.17 14.38	2.107 2.312 2.548	2.11 2.32 2.59	*	0.003 0.008 0.042		0.1 0.3 1.6		

\* Outside of the limits of Edmister's correlation.

#### Comparison of the Generalized Correlations of Bleich and Edmister with Original Data

			$c_p - c_w$		Difference		% Deviation	
Tr	<u> </u>	Calculated	Bleich	Edmister	Bleich	Edmister	Bleich	Edmister
1.291	0.2028 1.006 1.397	2.306 4.28 5.91	2.30 4.35 6.10	2.31 4.13 5.70	-0.006 0.07 0.19	0.004 -0.15 -0.21	-0.3 1.6 3.2	0.2 -3.5 -3.6
1.746	0.2866 1.512 2.938 12.81	2.169 3.12 4.36 5.54	2.17 3.12 4.32 5.55	2.20 3.11 4.20	0.001 0.00 -0.04 0.01	0.031 -0.01 -0.16	0.05 0.0 -0.9 0.2	1.4 -0.3 -3.7
2.291	0.380 1.260 3.19	2.107 2.395 3.04	2.10 2.40 3.03	2.15 2.44 3.10	-0.007 0.005 -0.01	0.043 0.045 0.06	-0.3 0.2 -0.3	2.0 1.9 2.0
3.38	1.139 5.09 12.01	2.128 2.551 3.05	2.11 2.55 3.10	₩ ₩ ₩	-0.018 -0.001 0.05		-0.8 -0.04 1.6	

#### ETHANE

\* Outside of the limits of Edmister's correlation.

#### Comparison of the Generalized Correlations of Bleich and Edmister with Original Data

		Cp	, - C <sub>V</sub>		Diff	erence	2 Devi	ation
Tr	p_r	Calculated	Bleich	<u>Edmister</u>	Bleich	Edmister	<u>Bleich</u>	<u>Edmister</u>
1.291	0.819 1.260 1.458	3•75 5•38 6•30	3.76 5.40 6.35	3.60 5.10 5.90	0.01 0.02 0.05	-0.15 -0.28 -0.40	0.3 0.4 0.8	-0.2 -5.2 -6.3
1.892	0.448 0.891 1.882 4.48 11.72	2.225 2.478 3.10 4.60 5.71	2.22 2.48 3.13 4.62 5.40	2.25 2.50 3.10 *	-0.005 0.002 0.03 0.02 -0.31	0.025 0.022 0.0	-0.2 0.1 1.0 0.4 -5.4	1.1 0.9 0.0
2.192	0.787 2.258 3.20	2.273 2.836 3.19	2.27 2.85 3.18	2.33 2.90 3.25	-0.003 0.014 -0.01	0.057 0.064 0.06	-0.1 0.5 -0.3	2.5 2.3 1.9
2.702	0.796 2.891 13.36	2•340 2•587 3•73	2.15 2.58 3.80	* *	-0.19 -0.007 0.07		-8.1 -0.3 1.9	

#### PROPANE

\* Outside of the limits of Edmister's correlation.

#### Comparison of the Generalized Correlations of Bleich and Edmister with Original Data

		Cp	, - C <sub>V</sub>	an a	Diff	erence	& Deviation	
<u> </u>	p <sub>r</sub>	Calculated	Bleich	<u>Edmister</u>	Bleich	<u>Edmister</u>	Bleich	Edmister
1.176	0.2097 0.884 1.100	2.449 5.23 6.91	2.44 5.35 7.10	2.45 4.95 6.30	-0.009 0.12 0.19	0.001 -0.28 -0.61	-0.4 2.3 2.7	0.04 -5.4 -8.8
1.647	0.302 1.429 3.98	2.219 3.31 5.90	2.21 3.30 5.90	2.24 3.27 5.60	-0.009 -0.01 0.00	0.021 -0.04 -0.30	-0.4 -0.3 0.0	0.9 -1.2 -5.1
2.117	0.392 0.976 1.954 13.91	2.113 2.376 2.793 5.16	2.12 2.37 2.79 4.82	2.18 2.42 2.85 *	0.007 -0.006 -0.003 -0.34	0.067 0.044 0.057	0.3 -0.3 -0.1 -6.6	3.2 1.9 2.0
3.06	1.449 6.52 12.87	2.209 2.868 3.42	2.20 2.87 3.40	*	-0.009 0.002 -0.02		-0.4 0.1 -0.6	

#### <u>n-BUTANE</u>

\* Outside of the limits of Edmister's correlation.

#### Comparison of the Generalized Correlations of Bleich and Edmister with Data of Deming and Shupe for Nitrogen

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Nitrog	sen t <sub>c</sub> =	-147.1	oc. p <sub>c</sub>	= 33.5 atm.	<b>_</b>			
				°p	- c <sub>v</sub>		S De	viation
t(°C)	p(psia)	Tr	<b>p</b>	Deming & Shupe	<u>Bleich</u>	Edmister	Bleich	Edmister
-70	20 100 500	1.61	0.600 2.985 14.925	2.44 5.51 5.08	2•5 5•35 5•4	2.5 5.1 *	2.5 - 2.9 6.3	2.5 -7.4
50	20 100 500	2.56	0.600 2.985 14.925	2.14 2.72 3.62	2.12 2.69 4.15	* * *	- 0.9 - 1.1 14.6	
400	100 300 500	5.34	2.985 8.955 14.925	2.09 2.18 2.29	2.11 2.32 2.49	<b>음</b> 분 상	1.0 6.4 8.7	

\* Outside of the limits of Edmister's correlation.

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#### Comparison of the Generalized Correlations of Bleich and Edmister with Data of Deming and Shupe for Carbon Monoxide

Carbon	Monoxide	t <sub>c</sub> =	-139°C.	•				
				<sup>C</sup> ي	- C <sub>y</sub>		% De	viation
t(°C)	<u>p(psia)</u>	<u> </u>	p	Deming & Shupe	Bleich	<u>Edmister</u>	Bleich	<u>Edmister</u>
-50	25 100 400	1.66	0.714 2.86 11.43	2.51 4.46 5.10	2.57 4.82 5.82	2.57 4.65 *	2.4 8.1 14.1	2.4 4.3
50	25 100 500	2.41	0.714 2.86 14.29	2.22 2.86 3.62	2.18 2.90 4.33	2.25 2.90 *	- 1.8 - 2.4 19.6	1.4 1.4
300	100 300 500	4.27	2.86 8.57 14.29	2.24 2.59 2.73	2.17 2.50 2.80	*	- 3.1 - 3.5 2.6	

\* Outside of the limits of Edmister's correlation.

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#### NOTATION

¢p	Heat capacity at constant pressure, molal basis - Btu/#-Mol-°F
°p	Specific heat at constant pressure, weight basis - Btu/#- <sup>O</sup> F
<b>C</b> <sup>*</sup> <sub>p</sub>	Heat capacity at constant pressure of a gas exhibiting ideal behavior, molal basis Btu/#-Mol- <sup>O</sup> F
C <sub>V</sub>	Heat capacity at constant volume, molal basis - Btu/#-Mol- <sup>O</sup> F
° <sub>v</sub>	Specific heat at constant volume, weight basis - Btu/#- <sup>O</sup> F
C#	Heat capacity at constant volume of a gas exhibiting ideal behavior, molal basis Btu/#-Mol-°F
p, P	Absolute pressure
T	Absolute temperature
t	Temperature - °C. or °F.
R	Universal gas constant
V	Molal volume
sub c	At critical conditions
sub r	At reduced conditions
5	Lewis and Bandall volume residual quantity
A <sub>o</sub> , B <sub>o</sub> , C a, b, c, c	r

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